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Fakulta strojní

Heat Generation in MRE under dynamic loading.

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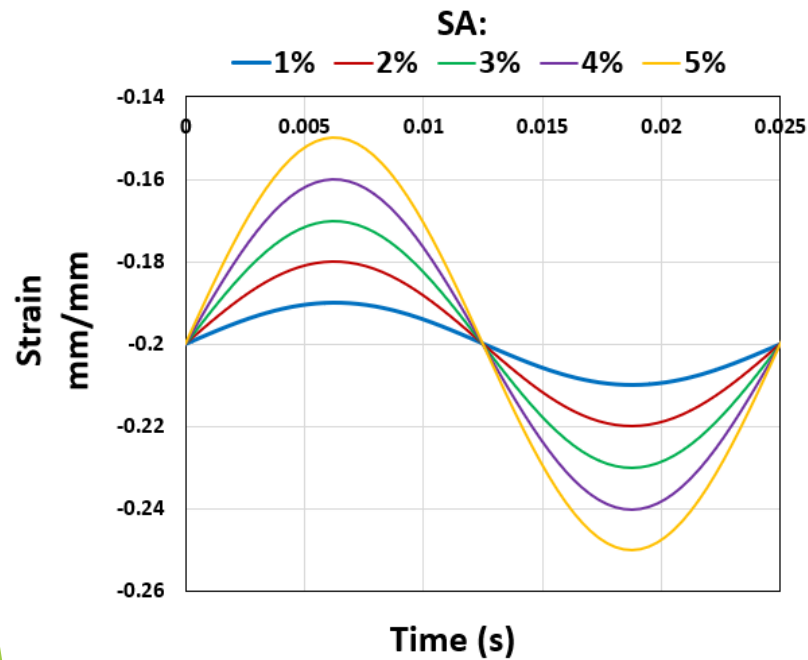
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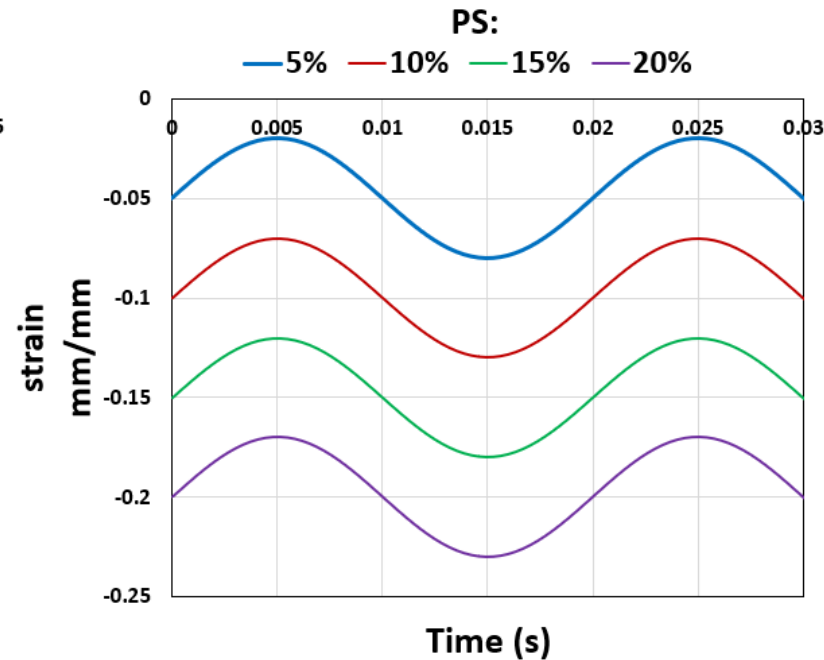
Experimental part: Dynamic Load.

- ▶ Dynamic tests were performed at different strain amplitudes (SA), pre-strains (PS) and frequencies (F) according to the shown groups for two hours.

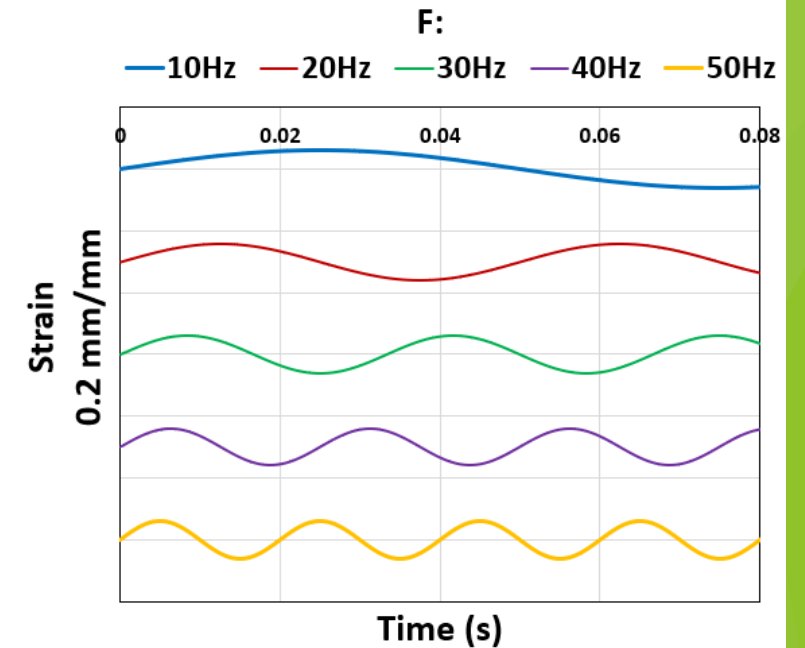
Group1: PS = 20%, F = 40Hz.



Group2: SA = 3%, F = 50Hz.



Group3: SA = 3%, PS = 20%.



Experimental part: Results.

- ▶ **Dissipated energy** is measured from stress strain hysteresis loops (J/m^3).

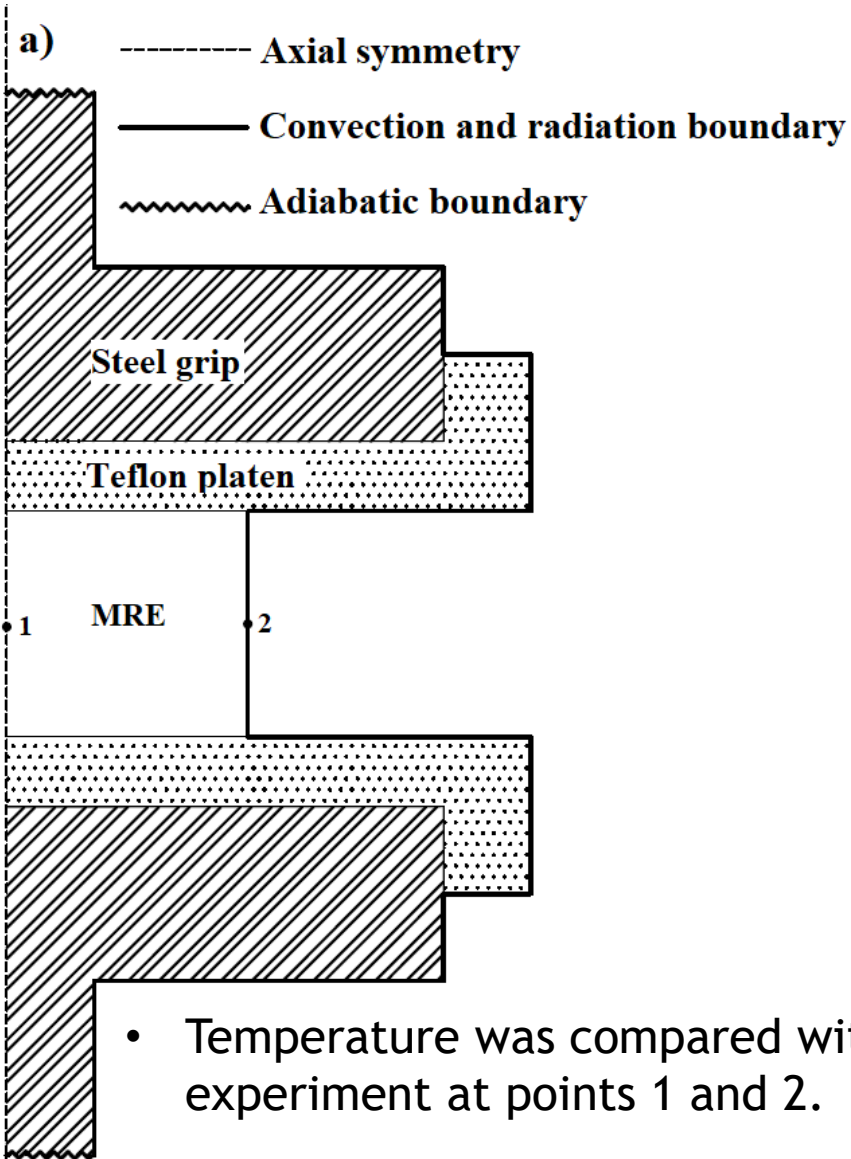
$$Q_{diss} = \int_0^{t1} \sigma(t) \dot{\epsilon}(t) dt$$

- ▶ **Sample Surface Temperature** was measured by using of infrared Camera.
- ▶ **Sample Internal Temperature** was measured by thermocouple.
- ▶ **Conversion ratios** were calculated by using the measured temperature field, at each testing case. According to the following equation:

$$\eta \dot{q}_{diss} = \frac{\rho C_p V \Delta T}{t} + 2 \frac{T_s - T_\infty}{R_t} + A \left(h_a (T_s - T_\infty) + \delta \gamma (T_s^4 - T_\infty^4) \right)$$

Where, η is the conversion ratio and represents the part of dissipated power which transferred to heat. And \dot{q}_{diss} is the total dissipated power in (W).

Simulation: Geometry, Boundary Conditions and parameters.



Material properties:

material	Emissivity (δ)	Conductivity (κ) $\left(\frac{\text{W}}{\text{m}\cdot\text{K}}\right)$	Specific heat (C_p) $\left(\frac{\text{J}}{\text{kg}\cdot\text{K}}\right)$
MRE	0.95	0.775	585
steel	0.22 [1]	22 [2]	475 [2]
Teflon	0.85 [1]	0.24 [2]	1050 [2]

Simulation: variables and functions.

Component 1 (comp1)

- Definitions
 - Variables 1
 - SA_1% (SA1)
 - SA_2% (SA2)
 - SA_3% (SA3)
 - SA_4% (SA4)
 - SA_5% (SA5)
 - PS_5% (PS5)
 - PS_10% (PS10)
 - PS_15% (PS15)
 - PS_20% (PS20)
 - F_10HZ (F10)
 - F_20HZ (F20)
 - F_30HZ (F30)
 - F_40HZ (F40)
 - F_50HZ (F50)

Dissipated power from experimental data.

Name	Expression	Unit
h_cylinder1	if(T>T_inf,(0.025/0.01295)*(0.825+17.04*(0.0138^3*(T-T_inf)/T_inf)^(1/6))^2,1) [W/(m^2)*K]	W/(m^2.K)
h_cylinder2	if(T>T_inf,(0.025/0.048)*(0.825+17.04*(0.048^3*(T-T_inf)/T_inf)^(1/6))^2,1) [W/(m^2)*K]	W/(m^2.K)
h_lower1	if(T>T_inf,1.5*((T-T_inf)/((0.0146)^2*T_inf))^(1/5),1) [W/(m^2)*K]	W/(m^2.K)
h_lower2	if(T>T_inf,1.5*((T-T_inf)/((0.0117)^2*T_inf))^(1/5),1) [W/(m^2)*K]	W/(m^2.K)
h_upper1	if(T>T_inf,5.15*((T-T_inf)/(0.0146*T_inf))^(1/4),1) [W/(m^2)*K]	W/(m^2.K)
h_upper2	if(T>T_inf,5.15*((T-T_inf)/(0.01173*T_inf))^(1/4),1) [W/(m^2)*K]	W/(m^2.K)
Q_int	eta*SA1(t)*(0.91==eta)+eta*SA2(t)*(0.84==eta)+eta*SA3(t)*(0.82==eta)+eta*SA3(t)*(0.82==et...	

Convection coefficients were written according to the following equations [1]:

$$h_{cyl} = \frac{0.025}{0.01295} \left[0.825 + 17.04 \left(L^3 \frac{(T_s - T_\infty)}{T_\infty} \right)^{1/6} \right]^2$$

$$h_u = 5.15 \left(\frac{T_s - T_\infty}{L T_\infty} \right)^{1/4}$$

$$h_l = 1.5 \left(\frac{T_s - T_\infty}{L^2 T_\infty} \right)^{1/5}$$

Where L is the characteristic length

$$\frac{Volume}{Area} \text{ or } \frac{Area}{Perimeter}$$

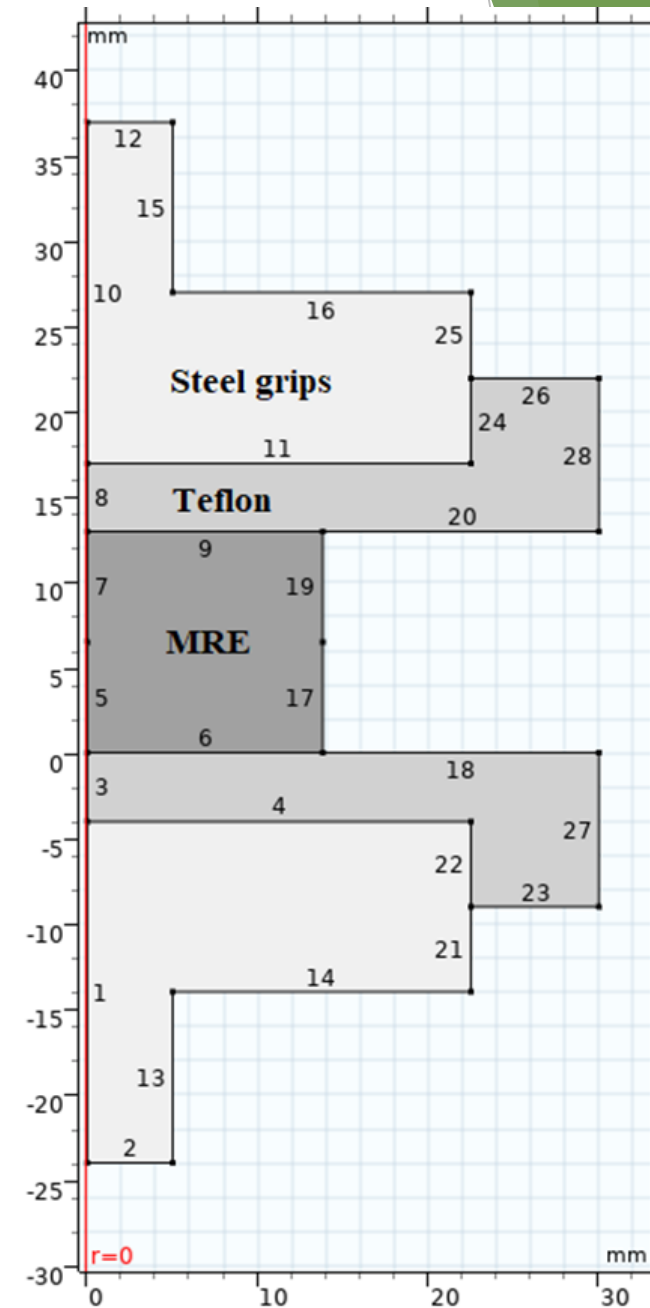
Simulation: Heat transfer in solids.

Heat Transfer in Solids (ht)

- ▷ Solid (Sample)
- ▷ Initial Values 1
- ▷ Axial Symmetry 1
- ▷ Thermal Insulation 1
- ▷ Solid (Teflon)
- ▷ Solid (Steel)
- ▷ Heat Source (Q_int)
- ▷ Heat Flux (h_cylinder1)
- ▷ Heat Flux (h_cylinder2)
- ▷ Heat Flux (h_lower1)
- ▷ Heat Flux (h_lower2)
- ▷ Heat Flux (h_upper1)
- ▷ Heat Flux (h_upper2)

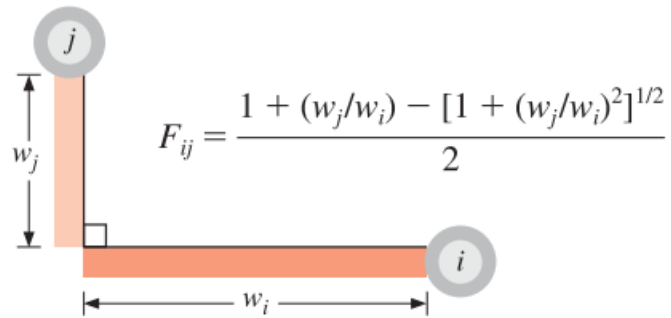
Coefficient:	Boundary No.
h_cylinder1	17, 19
h_cylinder2	27, 28
h_lower1	14,23
h_lower2	20
h_upper1	16, 26
h_upper2	18

- **Thermal contact resistance** is ignored as the Teflon surface is soft and in pressure contact with steel and MRE [1].



Simulation: Surface to surface radiation.

Radiation between MRE sample and Teflon platens was proved to be significant by using the following equation to calculate the view factor between them:

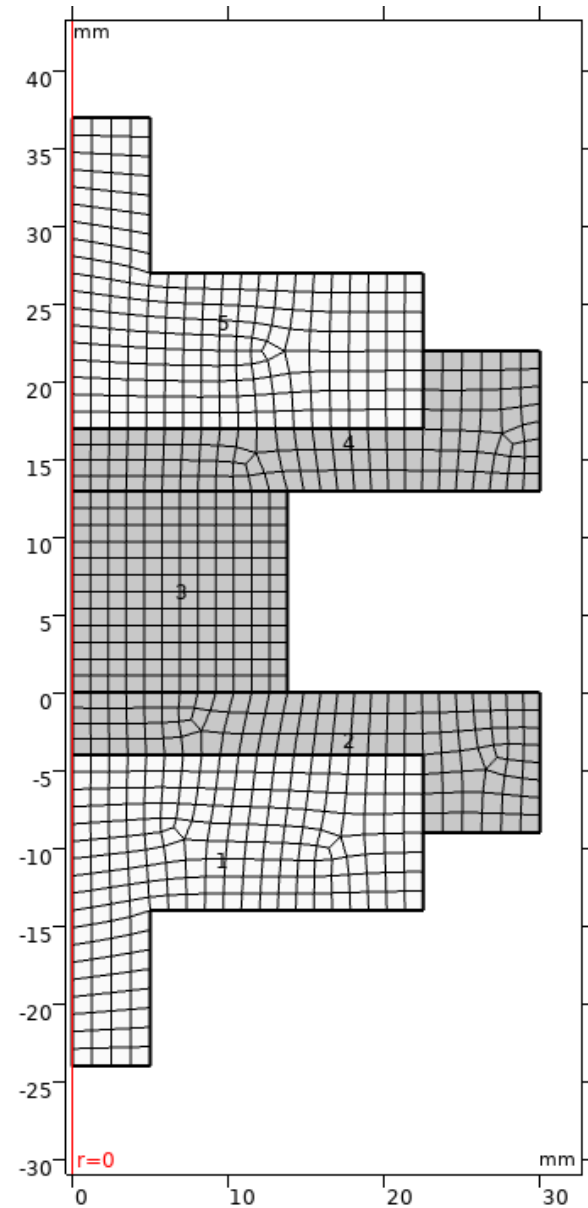


Therefore, a Surface to surface Radiation physics was used to calculate both radiations:

1. To ambient.
2. Between surfaces.

- ☀ Surface-to-Surface Radiation (*rad*)
 - ▷ ☒ Diffuse Surface 1
 - ▷ ☒ Initial Values 1
 - ▷ ☒ Axial Symmetry 1
 - ▷ ☒ Diffuse Surface (MRE)
 - ▷ ☒ Diffuse Surface (Teflon)
 - ▷ ☒ Diffuse Surface (Steel grips)
 - ▷ ● Opacity 1

Simulation: Mesh.

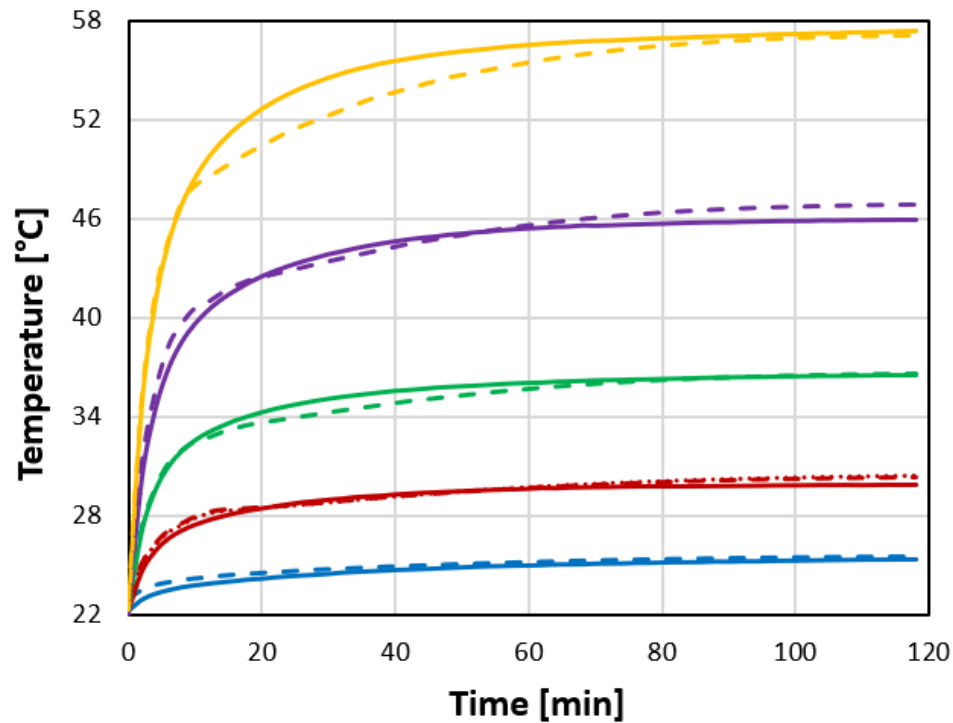


Results: At variable Strain Amplitudes (Group1):

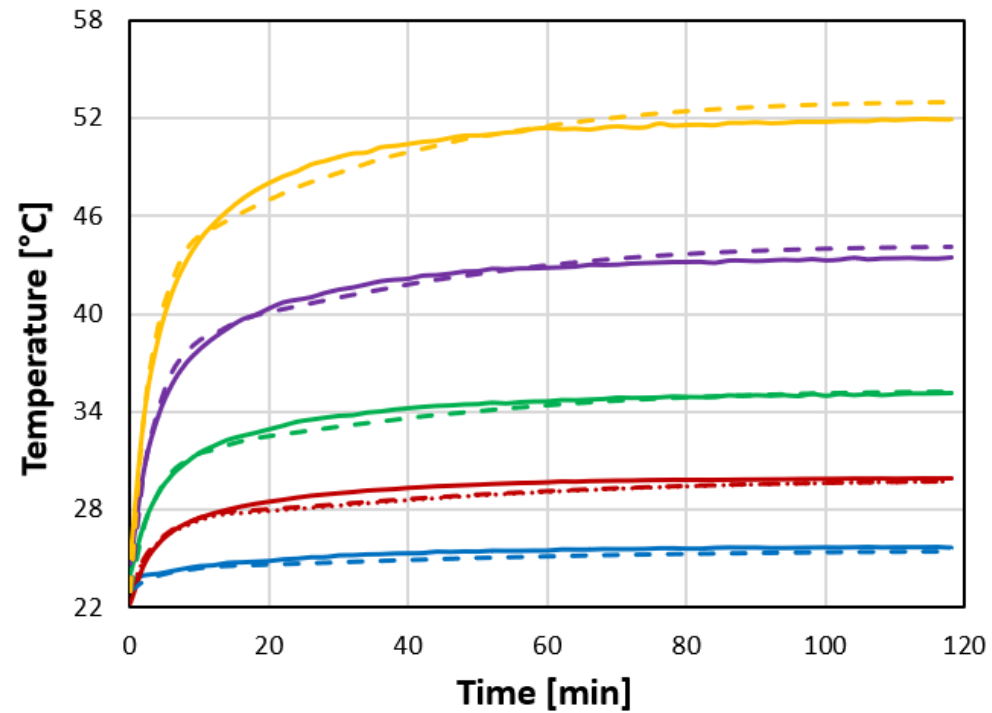
Group1: PS = 20%, F = 40Hz.

SA:

— 1% — 2% — 3% — 4% — 5%



Internal temperature



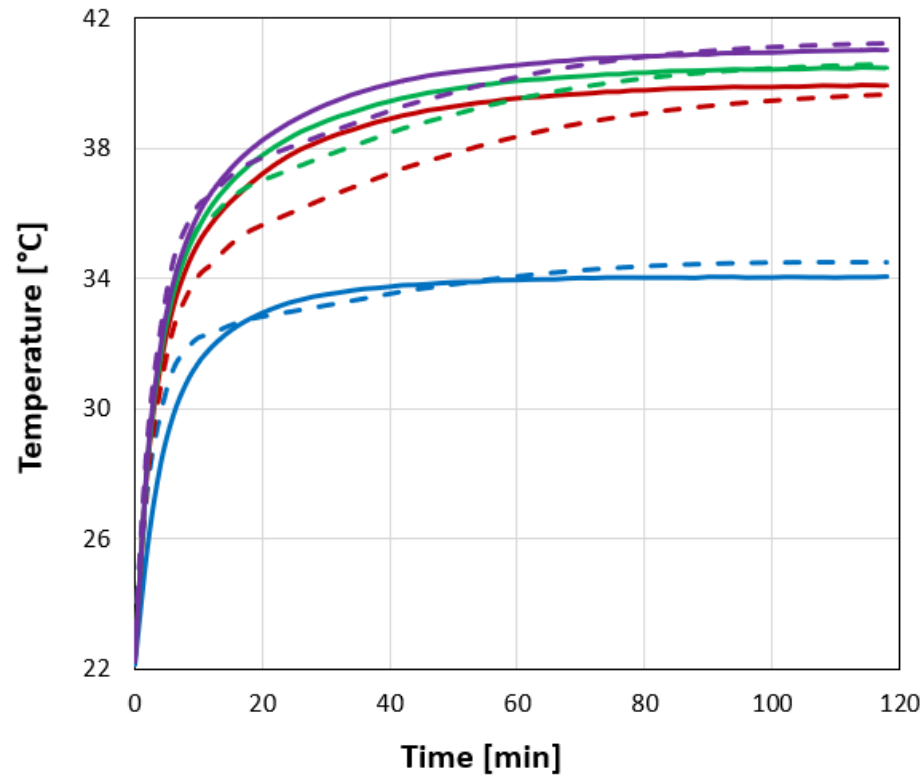
Surface temperature

Results: At variable Pre-strains (Group2):

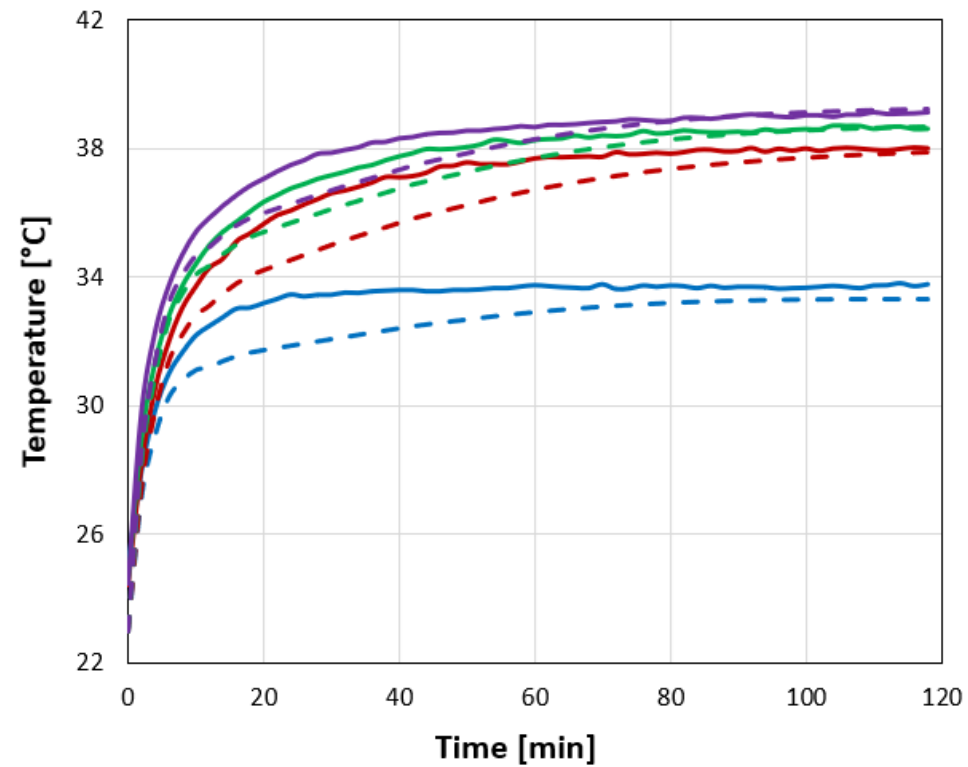
Group2: SA = 3%, F = 50Hz.

PS:

—5% —10% —15% —20%



Internal temperature



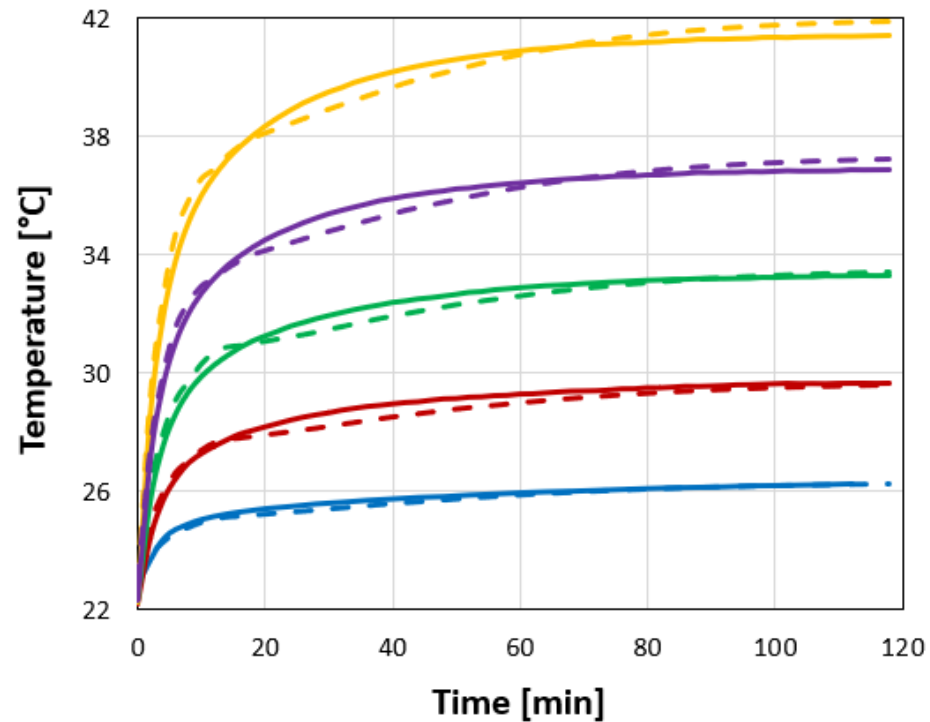
Surface temperature

Results: At variable Frequencies (Group3):

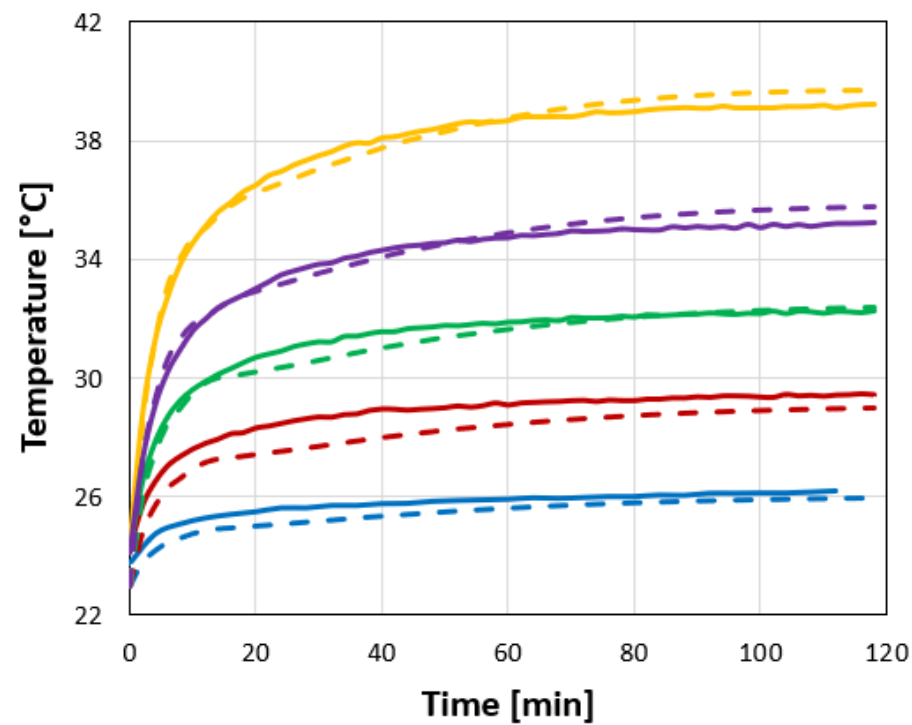
Group3: SA = 3%, PS = 20%.

F:

— 10Hz — 20Hz — 30Hz — 40Hz — 50Hz



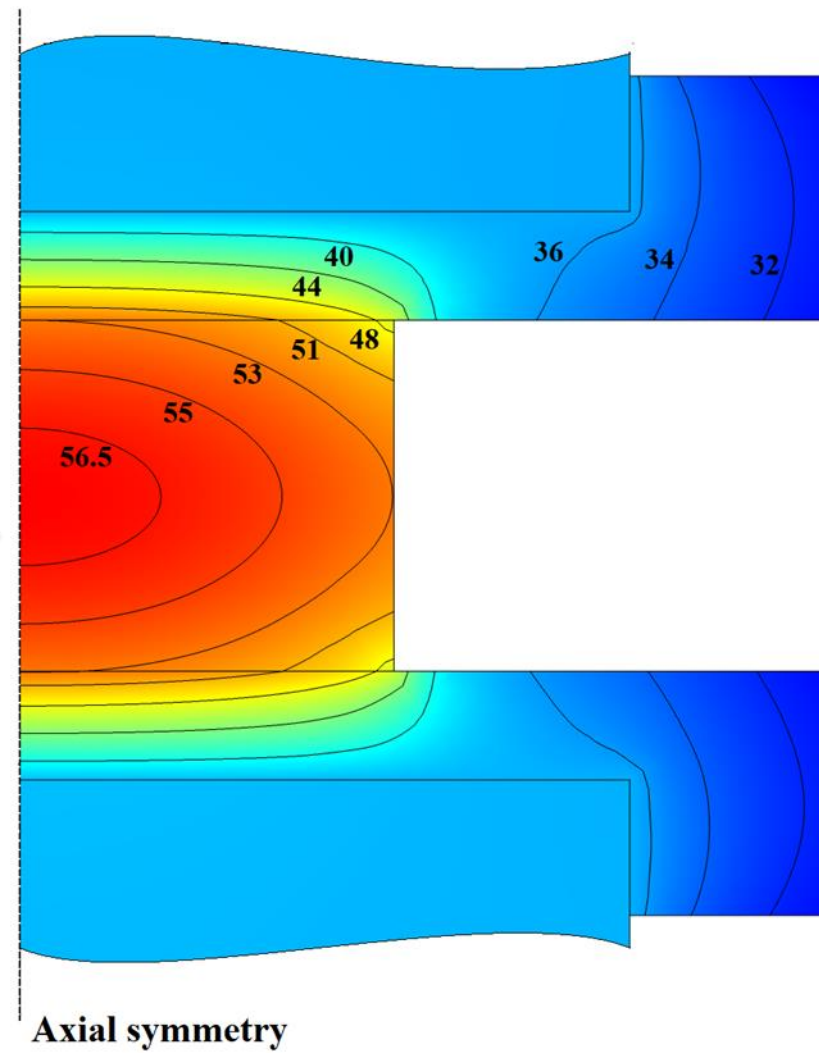
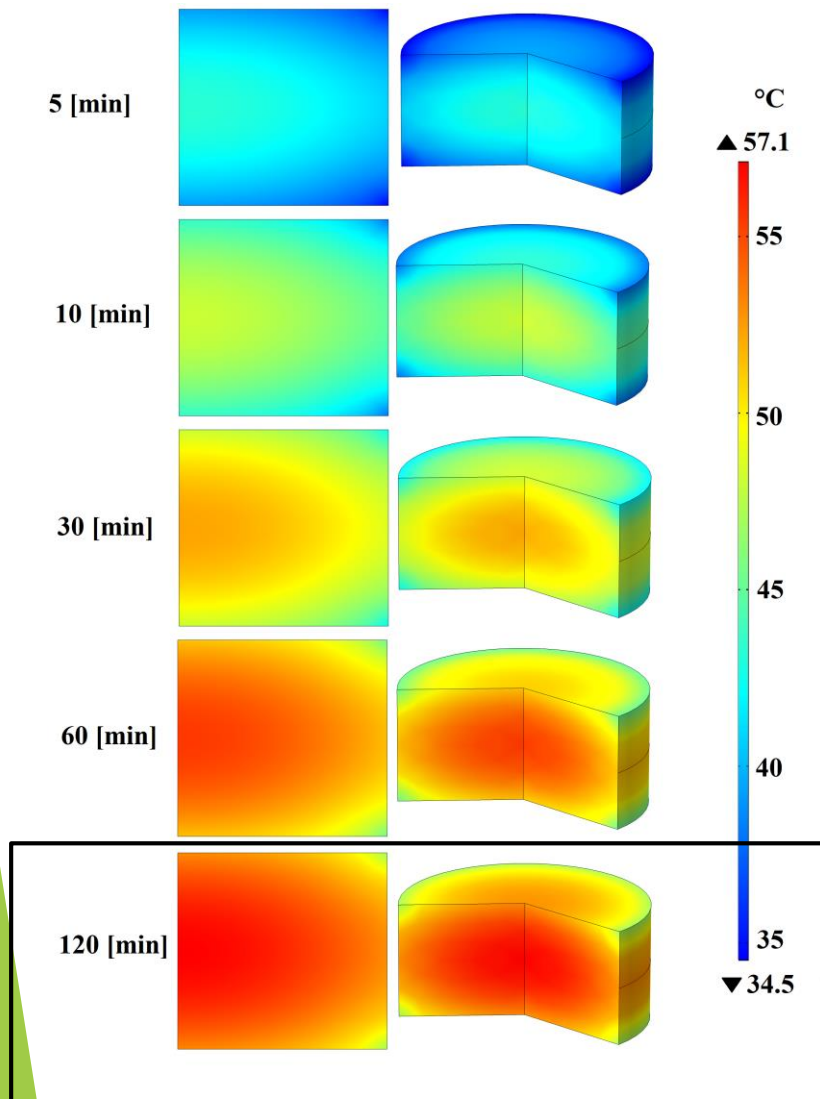
Internal temperature



Surface temperature

Results: Temperature Distribution.

At $F = 40\text{Hz}$, $PS = 20\%$, $SA = 5\%$ and time = (5 to 120)min.



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References:

[1]: Fundamentals of Heat and Mass Transfer, FRANK P. INCROPERA.

[2]: COMSOL Multiphysics 5.4 library.

Thanks for your attention.